

# Technical challenges linked to HVDC cable's development

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### Content

- No introduction → read the article!
- Fundamentals of extruded cables
- Accessories and field control
- Fundamentals of MI cable
- Conclusions



# FUNDAMENTALS OF EXTRUDED CABLES



#### Different types of cables





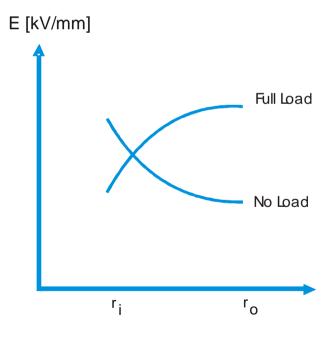
- MI (Mass Impregnated) first AC but also for DC
- LPOF (Low Pressure Oil Filled) for both AC and DC
- HPGF (High Pressure Gas Filled) for AC
- HPFF (High Pressure Fluid Filled) for AC
- EPR for AC
- PE for AC (DC?)
- XLPE for AC and DC (HVDC-Light)
  - Filled polymers for DC (Nanocomposites)
    - GIL (Gas Insulated Lines-SF6) for AC
    - **Superconducting Cables**



## Challenges with extruded HVDC cables Characteristics of an ideal HVDC insulation material

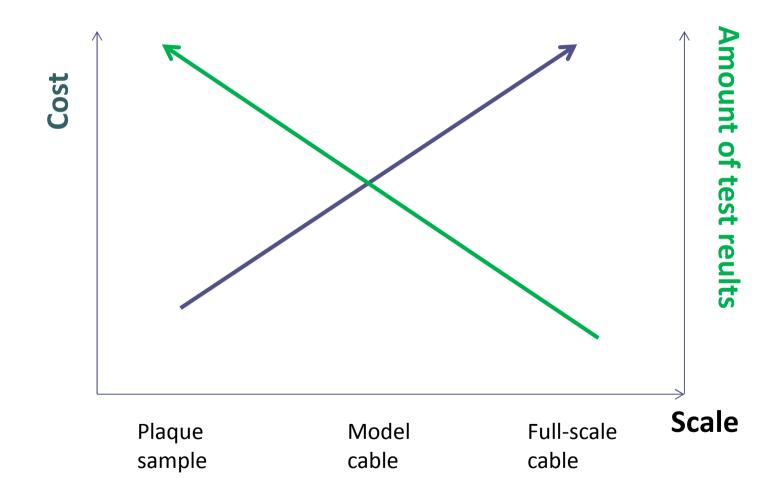
- Electrical properties:
  - High electrical withstand
  - Low DC conductivity -> Low thermal losses
  - Low space charge accumulation -> Electric field
  - Electrical aging
- Other properties (less discussed):
  - Thermal/mechanical aging
  - Processability
  - Quality control: material and cable
  - Chemically stable
  - Good mechanical properties
  - Not harmful to environment
  - Cost of material and production

- ....





#### Challenges with extruded HVDC cables Characteristics of an ideal HVDC insulation material





#### Challenges with extruded HVDC cables Material characterization: Plaque samples vs. cables

- Major differences between plaque samples and cables:
  - Different process condition
  - Cylindrical geometry of cables
  - Insulation thickness
  - Electrode material
  - Temperature gradient

...

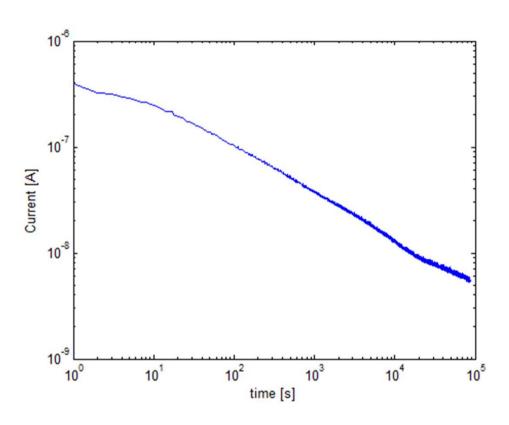
- Plaque sample results can be dominated by interface physics at the electrodes.
- One needs to be careful when making strong conclusions based on plaque sample results.



#### Challenges with extruded HVDC cables

#### Material characterization: Low DC conductivity

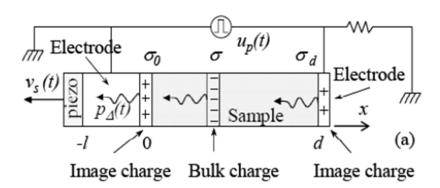
- Plaque sample sensitive to:
  - Sample thickness
  - Process condition
  - Heat treatment
  - Electrode material
  - Interface contact
  - Humidity
  - ...
- The current does not reach steady state.
- Valuable but not easy to interpret.
- Same is valid for space charge mesaurements.

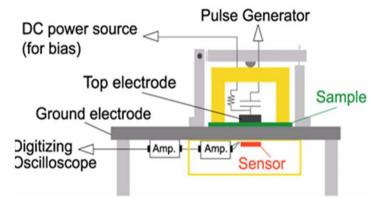




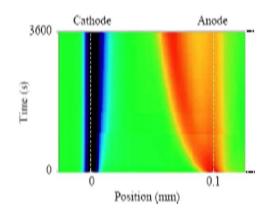
#### Challenges with extruded HVDC cables

#### Material characterization: Space charge (PEA)





- Pulsed Electro-Acoustic (PEA) measurement:
  - Mainly on plaque samples
- PEA on thick cables:
  - Cylindtrical geometry -> Distortion
  - Thick insulation -> Damping
  - Acoustic signal speed changes by temperature; temperature gradient distorts the signal strongly.
  - Reflection from multiple layers.



from: www.5lab.co.jp

and: Tanaka et. all."Material challenge of MgO/LDPE nanocomposites for high field electrical insulation", Cigre 2008



#### Challenges with extruded HVDC cables

#### Modelling and design

#### Generic:

for each charge carrier:

$$\frac{\partial n_k}{\partial t} + \frac{\partial j_k}{\partial x} = R_k(n_l)$$

$$j_k = n_k v_k - D_k \frac{\partial n_k}{\partial x}$$

$$v_k = \mu_k E$$

$$j = \sum_k q_k j_k$$

Boundary conditions: A function of field and tempertature for each carrier.

- Complicated.
- Large number of parameters required.
- Sensitive to the parameters.

#### Pragmatic:

Conductivity as a function:

- Simple, fast and convergent
- Few parameters required
- Reasonable results
- Does not simulate all reality but a very useful model

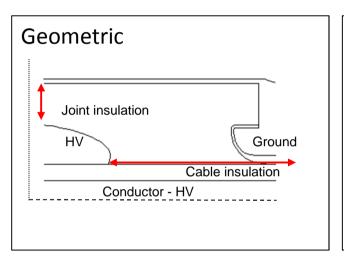


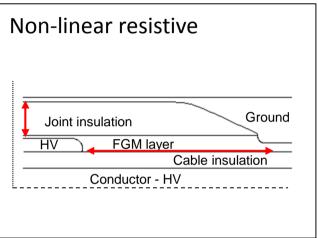
# ACCESSORIES AND FIELD CONTROL



#### DC-Field control

#### Geometry example





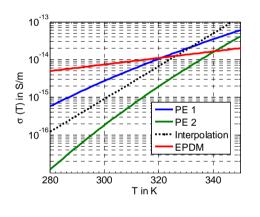
- Geometry of conducting parts according to impulse stress and allowed interface fields
- Field control layer connects HV to ground
- Material properties to be chosen according to DC and impulse stress.

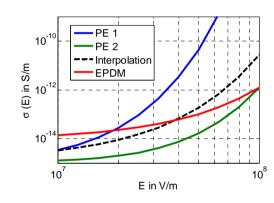


#### Electrothermal stresses in HVDC cable systems Wave shapes, material properties and simulation models

Conductivity is strongly Influenced by temperature and electric field

PE<sup>1</sup> and EPDM<sup>2</sup> (<sup>1</sup>Boggs et al, 2001, <sup>2</sup>relative to PE<sup>1</sup>)





- Heat conduction in the solid
  - Current in the conductor
  - Resistive losses in the insulation
- Electro thermal coupling is essential for DC field simulations!

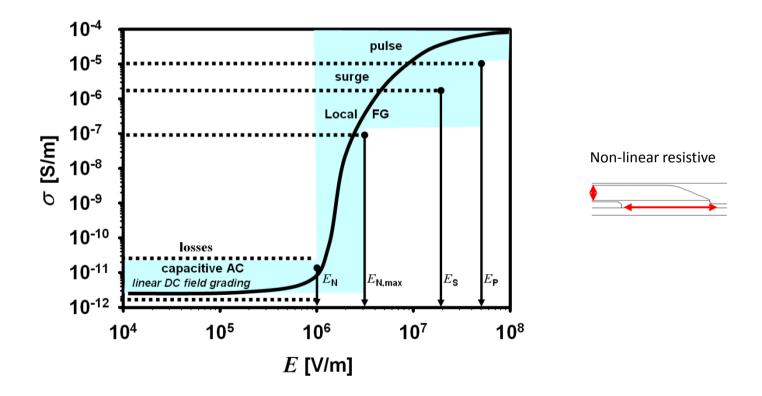
$$\nabla \cdot (\sigma(E, T)\nabla V) - \nabla \cdot \frac{\partial \varepsilon_0 \varepsilon_r \nabla V}{\partial t} = 0 \qquad \rho_M c_p \frac{\partial T}{\partial t} + \nabla (-\lambda \nabla T) = Q(E, I_0)$$



#### DC-Field control Material properties

#### Field grading material

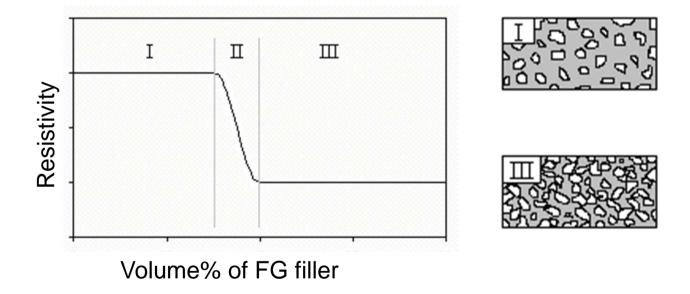
Non-linearity according to DC and impulse stress.



#### Field control

#### Non-linear resistivity / conductivity

- FGM consist of filler particles which form a network of contacts.
- 20-40 v% of particles

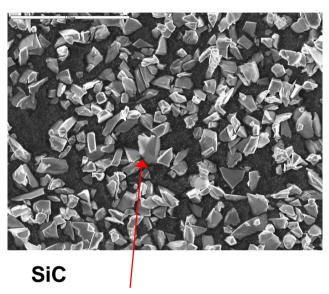


• In region 3 the electrical properties are determined by the particle material and the contacts between the particles.

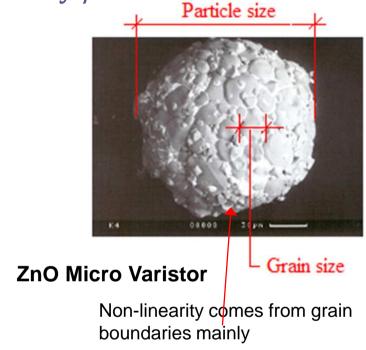


#### Field control

#### Non-linear resistivity / conductivity



Particle-Particle contact is non-linear



- In both cases the non-linearity is related to Schottky barriers
- Carbon black is also often used as a second filler, connecting the FG particles
- Other material concepts to arise

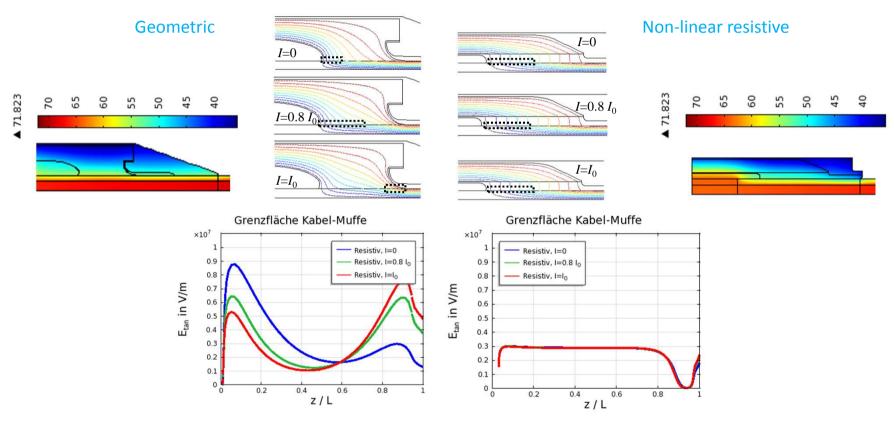




#### DC-Field control

#### Electric field distribution - comparison

Comparison of different load scenarios under DC voltage



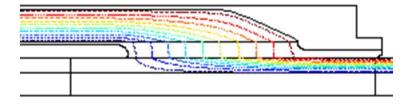
- Non-linear resistive layer dominates the field distribution
- Robust against variations in load and/or material properties, due to "adaptive resistive" control



#### DC-Field control

#### Electric field distribution - comparison

- Coupling of electrical and thermal material properties is essential to capture the dynamics/behaviour of HVDC accessories
- A layer of non-linear resistive field grading material leads to robust behaviour under DC stress.
- A layer of non-linear resistive field grading material gives a more even field distribution under DC stress.





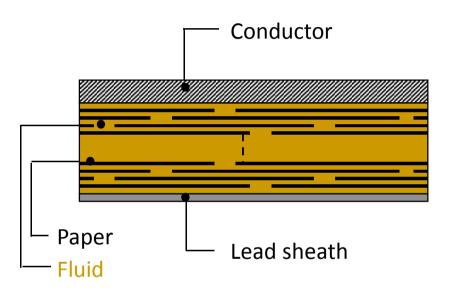
### **FUNDAMENTALS OF MI CABLE**



## MI Cable

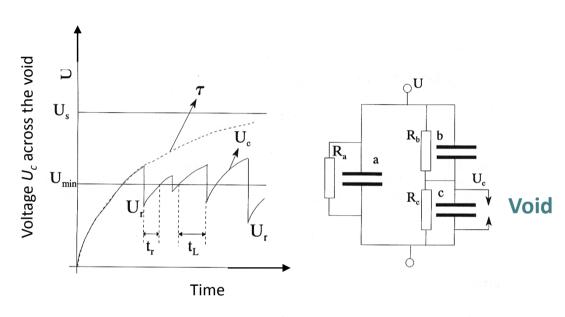


HVDC Mass Impregnated cable





## Partial Discharges at DC



One can calculate the discharge

- Repetition rate
- Magnitude

... of 1 void

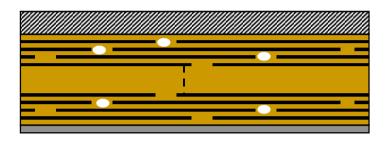
Model the hydrodynamic behaviour of the cable and one can calculate the discharge

- Repetition rate
- Magntiude

of the whole cable.

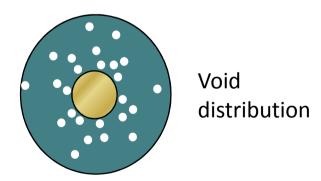


## Partial Discharges at DC - many voids



Voids can appear in in

- •butt-gaps
- between paper layers
- •inside paper

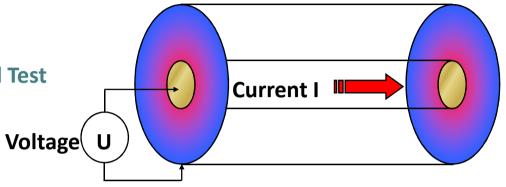


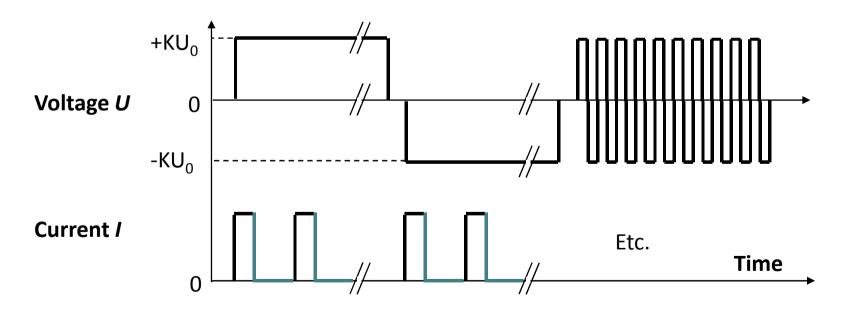


## Type Testing the HVDC - MI cable

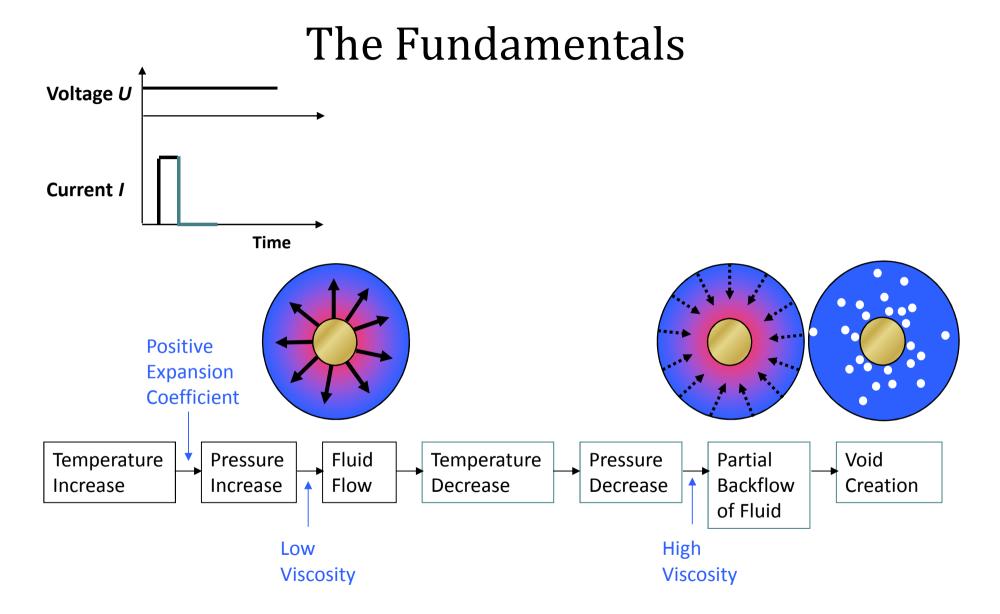
#### **Backbone of a Type Test:**

- Bending Test
- Load Cycle Test and Polarity Reversal Test
- Switching Surge Withstand test
- •Lightning Impulse Withstand Test
- •External Water Pressure Withstand Test
- Visual Inspection



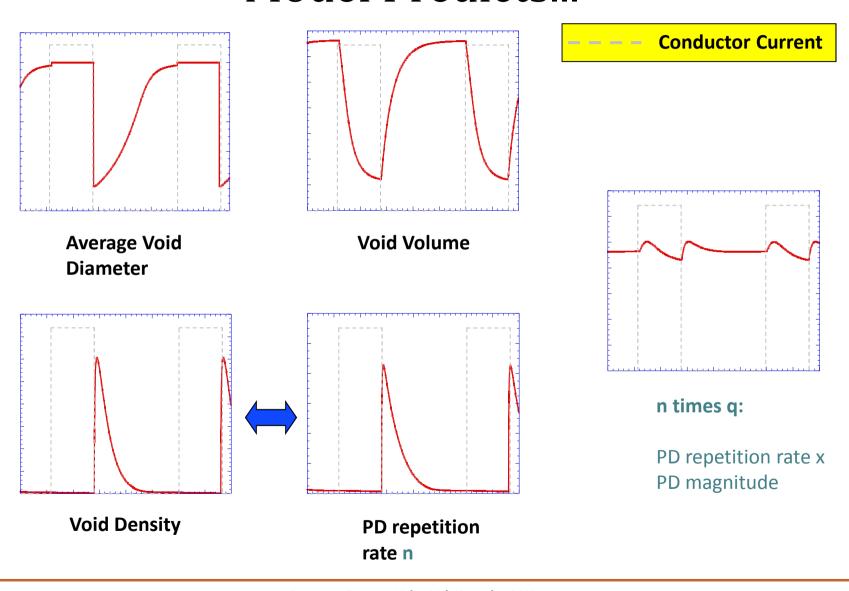








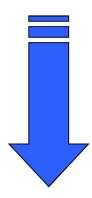
## Model Predicts...





## nq: repetition rate times magnitude

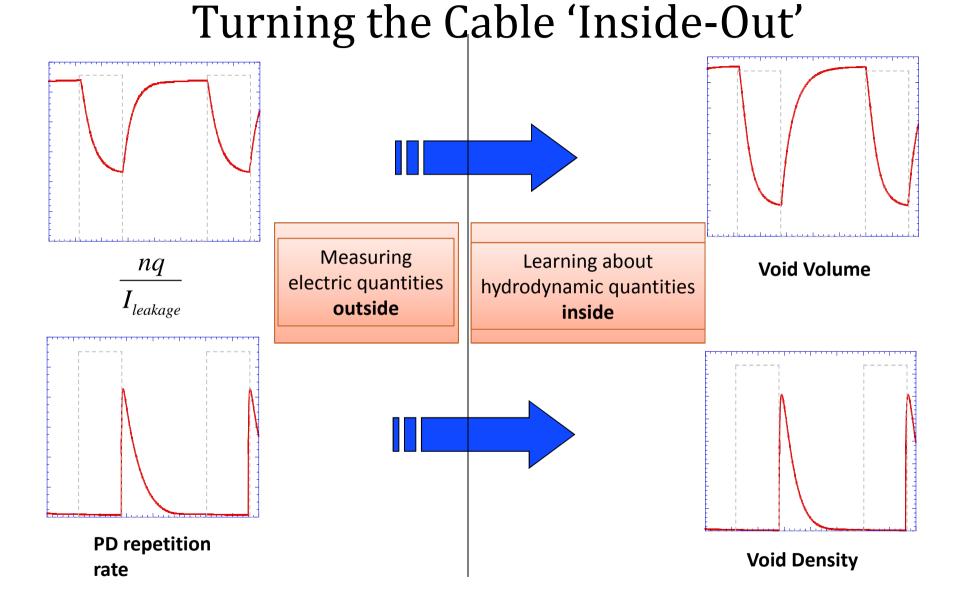
Does a physical meaning exist behind the measure nq?



$$\frac{nq}{I_{leakage}} \cong void \ volume$$







## **CONCLUSIONS**



## Conclusions

- The future faces increased voltages and powers
- Challenges:
  - Understanding the physics
  - Proper measurement principles
  - Upscaling
  - Quality Assurance and Quality Control